#### Title

## Experimental Analysis of the Wall Collision of Irregular and Regular Shaped Non-Spherical Particles

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## **Introduction 1**

- Numerical predictions of dispersed two-phase flows rely generally on the assumption of spherical particles.
- However, in most practical situations and industrial processes the particles are irregular in shape or have a certain geometrical shape, (e.g. fibres, cylinders, discs, ...) or are even agglomerates.
- For modelling the motion of such non-particles in confined flows (i.e. pipes, cyclones, ...) the knowledge of the wall collision parameters (i.e. restitution and friction) is necessary.







## **Introduction 2**

Modelling the wall collision of non-spherical particles is essential for a reliable numerical calculation of particle-laden confined processes.

> Lagrangian treatment of nonspherical particle wall collisions

> > $ec{\omega}_{\scriptscriptstyle P,0}$

**Contact Point** 

۲<sub>C</sub>

## Regularly shaped nonspherical particles

- Tracking the orientation of the particles (Euler parameters or quaternions)
- ✓ Solving the impulse equations for non-spherical particles (Sommerfeld 2002)
   *u<sub>P,C</sub>*

# Irregular non-spherical particles

- ✓ Solve the wall collision process for a spherical particle
- Draw the values for restitution and friction from a PDF
- ✓ Requires experiments !!!

## **Introduction 3**

For modelling the wall collision of irregular non-spherical particles the basic equations for spherical particles are used (point mass):
 Non-sliding collision:

> Sliding collision:

$$u_{P2} = u_{P1} + \mu_{d} \epsilon_{x} (1+e) v_{P1}$$
$$v_{P2} = -e v_{P1}$$
$$w_{P2} = w_{P1} + \mu_{d} \epsilon_{z} (1+e) v_{P1}$$

$$\begin{split} &\omega_{P2}^{x} = \omega_{P1}^{x} - 5 \ \mu_{d} \ \epsilon_{z} \ \left(1 + e\right) \frac{v_{P1}}{D_{P}} \\ &\omega_{P2}^{y} = \omega_{P1}^{y} \\ &\omega_{P2}^{z} = \omega_{P1}^{z} + 5 \ \mu_{d} \ \epsilon_{x} \ \left(1 + e\right) \frac{v_{P1}}{D_{P}} \end{split}$$

Condition for non-sliding:

$$\left| u_{R1} \right| \le \frac{7}{2} \mu_0 \left( 1 + e \right) v_{P1}$$







- Photron High Speed Video Camera,
  FASTCAM SA4 RV operated at 60,000 fps (resolution 256 \* 192 Pixels)
   LED illumination back-lightning
   Telecentric lens of T80 series
- Magnification ratio of 1:1

> Summary of particle properties for the wall collision experiments

Material	Density (kg/m <sup>3</sup> )	Size Distribution Diameter (µm)	Mean size, VES (µm)	Sphericity
Cylinders *	2500	500	500	0.779
MC4 Duroplast	1500	250 - 350	300	0.773
Quartz Sand	2400	200 - 300	250	0.851

Cylinders (fishing rope): diameter 0.5 mm, length ~ 1.5 mm; axis ratio l/d=3





> Wall collision of an irregular particle (Duroplast particles MC-4, projection diameter 300  $\mu$ m,  $\psi$  = 0.773, velocity: 16.3 m/s)







#### vertical camera

Before and after collision





> Videos wall collision of cylindrical particles (Duroplast particles MC-4, projection diameter 300  $\mu$ m,  $\psi = 0.773$ , velocity: 16.3 m/s)

horizontal camera view

vertical camera view







The restitution ratios are determined from the ratio of the velocities obtained by the particle tracking routine:

$$e = \left| \frac{V_2}{V_1} \right|$$
  $e_n = \left| \frac{V_{y2}}{V_{y1}} \right|$   $e_t = \frac{V_{x2}}{V_{x1}}$ 

From the impulse equations for spherical particles the friction coefficient is obtained in the following way:

$$\mu = \frac{|V_{x1} - V_{x2}|}{(1+e) V_{y1}}$$





**Results Wall-Collision 1** 

> PDF's of normal restitution ratio for different impact angles (Quartz).



> Dependence of restitution and friction coefficients on the impact angle



> Dependence of total restitution coefficient on impact velocity:



**Results Wall-Collision 4** 



**PDF**`s of friction coefficient for different impact angles (MC-4).

![](_page_13_Figure_2.jpeg)

**The Second Seco** 

![](_page_14_Figure_2.jpeg)

For describing the dependence of mean values and standard deviation appropriate correlations are derived. The instantaneous values are drawn from a normal distribution. The wall collision process is calculated as for a spherical particle.

Wall collision of a cylindrical particle (cylinder diameter 500 μm, axis ratio L/D = 3, velocity: 16.3 m/s)

![](_page_15_Figure_2.jpeg)

![](_page_15_Picture_3.jpeg)

![](_page_15_Picture_5.jpeg)

> Videos wall collision of cylindrical particles

horizontal camera view

vertical camera view

![](_page_16_Picture_4.jpeg)

![](_page_16_Picture_5.jpeg)

![](_page_16_Picture_7.jpeg)

## **Comparison 1**

**Comparison of the results for the regular and irregular non-spherical particles** 

![](_page_17_Figure_2.jpeg)

## **Comparison 2**

**Comparison of the results for the regular and irregular non-spherical particles** 

![](_page_18_Figure_2.jpeg)

## **Conclusions / Outlook**

- A special test facility has been developed for analysing the wall collision process of non-spherical particles.
- The wall collision process was recorded by two perpendicularly installed high speed cameras.
- **The wall collision angle was varied between about 5 to 85 degree.**
- For each wall collision angle about 100 events were recorded and statistically evaluated.
- In the experiments regular and irregular shaped non-spherical particles with a size of several hundred microns were considered.
- Soth the normal restitution ratio and the friction coefficient decreased with increasing impact angle.
- The standard deviation of both parameters remarkably increased with decreasing impact angle.
- For the irregular particles a stochastic wall collision model was developed based on the PDF`s of the two parameters.
- Further experiments will be conducted for cylinders with different aspect ratio.

![](_page_19_Picture_10.jpeg)

![](_page_19_Picture_12.jpeg)